

OVERVIEW OF THIRD GENERATION SPACEBORNE X-BAND SYNTHETIC APERTURE RADAR (SAR)

Abstract

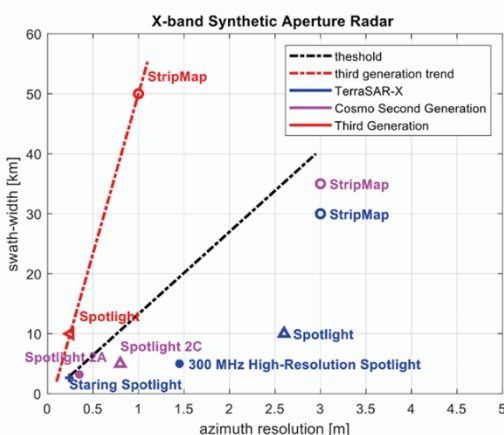
The deployment of advanced Synthetic Aperture Radar (SAR) observation capabilities from space represents a key element for military surveillance of border areas, support in critical logistic theatres and the collection of national security intelligence. Modern security and defence operational models use the Intelligence, Surveillance and Reconnaissance (ISR) function as one of the essential resources necessary to acquire a detailed and accurate situational picture, useful for obtaining valuable information to support decision-making, at a strategic level, operational and tactical. SAR satellites are one of the key solutions contributing to the implementation of an effective ISR capability, helping to enhance the protection of military forces and assets in the field.

In this context, it is clear that the quality of the information provided to the user obviously depends on the performance capabilities of the SAR system and, at most, on those of the instrument that constitutes its heart. This paper presents a few engineering solutions that can be evaluated in the perspective of a next generation of high-performance SAR instruments, in order to push performance beyond the current state of the art, improving the quality of intelligence and reconnaissance information and extending its operational purpose in support of national defence and security. In particular, the possibility of overcoming the current limits of the resolution achievable over wide swath widths is addressed as one of the key objectives to be pursued for these new generation advanced instruments. This paper describes an example of X-band SAR solution implementing this capability and its achievable image quality performance. The proposed example has no claim to exhaustiveness but it is useful in portending the significant repercussion that the architectural features presented could have for Imagery Intelligence (IMINT) applications.

Instrument Design

The current generation of spaceborne X-band SAR instruments can acquire microwave images with medium geometric resolution (~3 m) and medium swath width (~30 km) when operated in Stripmap. These instruments also offer acquisition modes to optimize resolution (Spotlight-based modes) or swath (ScanSAR-based modes), but improving one of these two parameters always comes at the expense of the other. On the other hand, modern remote sensing applications require improving both resolution and swath width, and complementing them with significant performance in terms of Noise Equivalent Sigma Zero (NESZ) and Distributed Target Ambiguity Ratio (2D-DTAR).

Figure 1 reports azimuth resolution vs. swath-width SAR performance of actual Instruments (Cosmo Second Generation and TerraSAR-X) vs. target performance for the third generation ones.



37 Figure 1 - X-band SAR Instruments swath-width vs. azimuth resolution: comparison between present and third
38 generation

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40 High geometric resolution performance over a large area can be achieved by applying innovative radar
41 acquisition techniques, such as Scan-On-Receive (SCORE) and Multiple Azimuth Processing (MAP),
42 which have been proposed in the recent years in order to overcome the theoretical trade-
43 offs limits constraining resolution and swath width in SAR instruments employing standard acquisition modes.
44 For example, by using these techniques the SAR can be designed to meet a target resolution of 1 m and a
45 swath of 50 km in StripMap and 10 km in Spotlight, establishing the conditions for exceeding the
46 performance limits of the current generation.

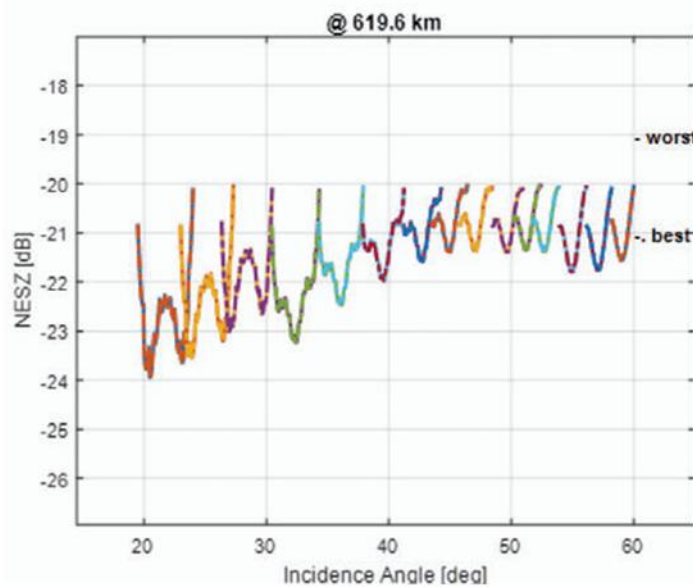
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48 Performance

49 The considered SAR instrument is assumed to be equipped with a planar active phased array antenna. In
50 addition, the proposed SAR instrument implements the following innovative acquisition techniques:

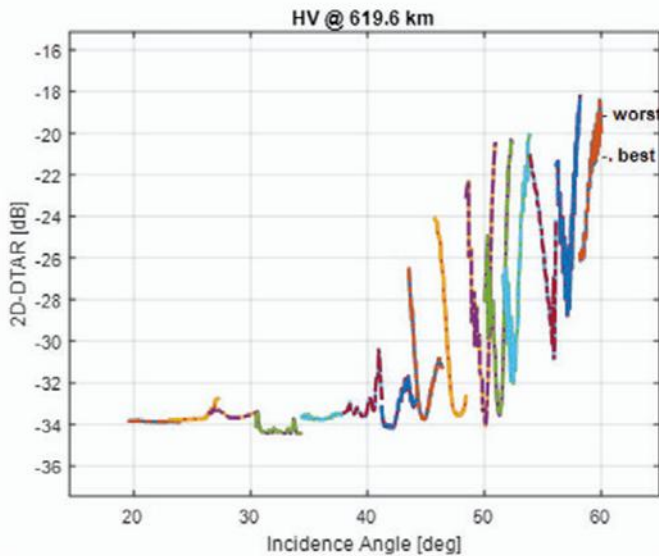
- 51 - Digital Beamforming (DBF) to implement Digital SCOREs, at the purpose of maximising the receive
52 antenna gain and therefore improving NESZ and range DTAR.
- 53 - AP implemented at digital level in SAR Electronic Sub-system (SES), for improving azimuth DTAR.

54 Figure 2 shows an example of values of NESZ achievable in Stripmap by implementing the
55 aforementioned techniques while Figure 3 shows the related curves of 2D-DTAR. The example refers to an
56 access region covering the range of incidence angles 20÷60 deg. These plots show that a worst value of NESZ
57 in the order of -20 dB and 2D-DTAR up to -18 dB are achievable over the considered access region. The
58 mentioned performance is computed at an orbital altitude of 619 km.



59 Figure 2: SAR Stripmap NESZ performance
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63 Figure 3: SAR Stripmap 2D-DTAR performance

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65 **Instrument Architecture**

66 The functional architecture of the considered instrument is shown in Figure 4. The instrument consists of
67 two main sub-systems: SAR Electronic Sub-system (SES) and SAR Antenna Sub-system (SAS).
68 Within SES, the digital unit (DGU) is conceived as a modular unit, developed to manage a large number of
69 receiver channels for supporting the acquisition techniques of SCORE and MAP. According to
70 a consolidated approach, this unit can be split in two echo-processing layers. A First Stage Processor (FSP)
71 module can implement a first level of processing including: signal sampling, filtering, and decimation,
72 signal compensation and digital beamforming. A Second Stage Processor (SSP) module can be used to
73 complete the processing of the FSP and to perform multi-channel calibration algorithms for supporting DBF
74 at the aim of implementing SCORE and echo data compression algorithm (Automatic BAQ developed by
75 TAS-I). SAS requires to be controlled by a dedicated Antenna Controller and Processor module (ACP). ACP
76 can be used also to control the internal SAR Instrument units and to communicate with the Platform (P/F).
77 The RF unit (RFU) within SES assures the signal conditioning to adapt the transmitted and received
78 signals between DGU and SAS. In between, a unit (SCSU) is required for splitting/combining and
79 switching the signals, and for managing redundancy paths. For each receiving path, RFU implements:
80 signal matching, filtering, amplification, gain control, and adaptive down-conversion schemes based on the
81 different observation modes of the instrument. The internal functions of SAS can be assumed to be
82 distributed among five assemblies: Radio Frequency, Power, Command and Control, Mechanical, and
83 Thermal assemblies. The electrical functions included in the first three assemblies can in turn be assigned to
84 the following set of units, which are typical of a SAR active phased array antenna: Tile Control Unit (TCU),
85 Tile Power Supply unit (TPSU), Electronic Front-End (EFE), True-time Delay Line (TDL), Radiating Board (RB),
86 Beamforming Network (BFN), and DC Harness.

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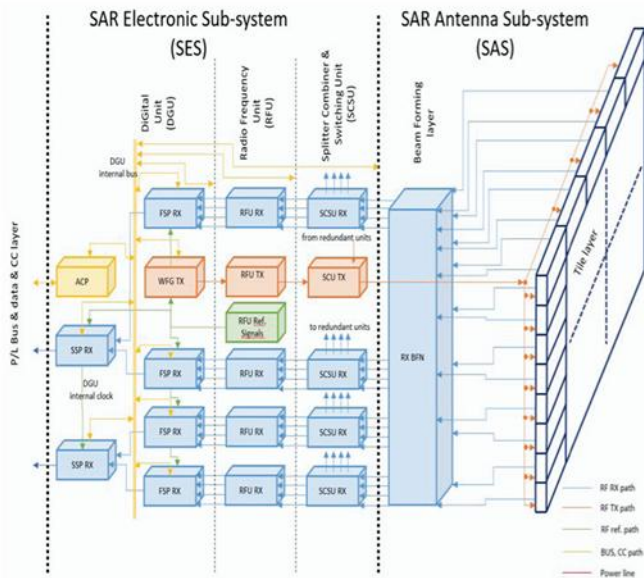


Figure 4: Example of SAR instrument functional architecture comprising two main subsystems: SES and SAS.

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