



26 maintenance costs [1]. Structures ranging from aircraft wings and fuselage panels to ship hulls and  
27 wind turbine blades are now routinely fabricated from these advanced materials.

28 However, the very attributes that make them desirable—their high strength and low weight—also  
29 render them inherently flexible and susceptible to vibrations. Even minor external disturbances, such  
30 as aerodynamic loads, acoustic noise, or wave impacts, can induce significant and persistent  
31 oscillations. These vibrations can lead to a host of detrimental effects, including structural fatigue,  
32 reduced operational precision, acoustic discomfort, and, in severe cases, catastrophic failure.  
33 Consequently, the implementation of robust vibration control strategies is not merely desirable but a  
34 critical requirement for ensuring the safety, performance, and longevity of laminated composite  
35 structures.

36 The challenge is further compounded by two inherent characteristics of composite materials: their  
37 susceptibility to damage and the presence of material uncertainties. Damage, such as delamination,  
38 matrix cracking, or fiber breakage, can occur during manufacturing or in-service operation and can  
39 drastically alter the structural stiffness and damping characteristics, thereby affecting the dynamic  
40 response and the efficacy of any control system. Simultaneously, material properties like fiber  
41 orientation, ply thickness, and constituent material moduli are often not precisely known due to  
42 manufacturing tolerances and inherent statistical variations. These uncertainties can lead to  
43 unpredictable dynamic behavior, making the design of reliable and robust vibration control systems a  
44 complex task.

45 Given the rapid growth of research in this domain, a structured review is necessary to consolidate  
46 recent findings and identify emerging trends. This literature review is therefore organized into four  
47 interconnected thematic areas to provide a holistic overview:

481. **Laminate Theories:** An examination of the various theoretical frameworks used to model the  
49 kinematic behavior of composite laminates, from simple Classical Laminate Theory to more  
50 sophisticated Higher-Order Shear Deformation Theories, highlighting their suitability for different  
51 structural configurations and control applications.
522. **Vibration Control Strategies:** A detailed discussion of the principal techniques employed for  
53 vibration suppression, distinguishing between passive methods (e.g., constrained layer damping, tuned

54 mass dampers) and active methods (e.g., using piezoelectric sensors and actuators), as well as  
55 emerging hybrid approaches.

563. **Modeling and Governing Equations:** A review of the fundamental principles, such as Hamilton's  
57 principle and the Euler-Lagrange equation, used to derive the equations of motion and boundary  
58 conditions for composite structures. The role of beam theories (e.g., Timoshenko, Euler-Bernoulli) and  
59 plate/shell theories in this context is also discussed.

604. **Applications and System Identification:** A focused analysis of recent studies that apply these  
61 modeling and control techniques to practical engineering structures in aerospace, naval, and civil  
62 engineering. This section pays particular attention to how researchers determine critical system  
63 parameters, such as natural frequencies, damping ratios, and mode shapes, especially when accounting  
64 for damaged states or uncertain material properties, and how they achieve system stabilization.

65 By synthesizing findings across these four areas, this review aims to provide a clear and concise  
66 picture of the current state-of-the-art in the vibration control of laminated composites under realistic  
67 conditions. The paper concludes by summarizing the key takeaways and outlining promising avenues  
68 for future research to address the remaining challenges in this critical field.

69

#### 70 **Different Lamination theory developed:**

71 In modern era with the increase in the application of laminated composite various laminated plates  
72 theories have been developed Classical theory of plates was initiated by Kirchhoff [2] in the nineteenth  
73 century, and then was continued by Love and Timoshenko [3] during the early twentieth century, but  
74 due to certain limitation these theories are not suited to derive all transverse shear stress of laminated  
75 composite plates, So Reissner [4] and Mindlin [5] in 1951 have given the idea of First-order shear  
76 deformation theory. In this theory a shear correction factor is needed to adjust the transverse shear  
77 stiffness and the accuracy of results of the FSDT will depend significantly on the shear correction  
78 factor. The limitations of the CLPT and the FSDT, A new higher-order shear deformation theory has  
79 proposed. higher-order shear deformation theory (HSDT) for laminated composite plates described in  
80 the journal published in 1988 by B.N.Pandya and T.Kant [6] .As the year passes away a Zig-zag  
81 theory for laminated plate has introduced to keep continuity in plate theories [7]. The application based  
82 development of laminated plate theories has proposed in 2011 by Khandan R Noroozi S,swell P

83 Vinney J [8]. Recently in 2013 F.Azhari , B.Boroomond &M Shahbati has given an idea for higher-  
84 order zig-zag theory for laminated composite plates [9].

### 85 **Vibration control of laminated composite structure:**

86 Composite structures are flexible in nature and vibrate with minimum disturbance. So, it is needed to  
87 control the vibration effect. Many researchers have done lot of experiment to vibration control like  
88 active and passive ways. Bailey and Hubbard Jr. in 1985 have purposed the control theory of  
89 distributed piezoelectric actuators [10]. Khdeir and Librescu has analyse the symmetric cross ply plate  
90 for vibration purpose with the help of higher-order shear deformation theory in 1988 [11]. The  
91 vibration control by piezoceramic actuator and piezo film sensor was done by Han et al [12] in 1997.  
92 As the year passes away the research on vibration control is going advance form e.g by Khdeir and  
93 Reddy [13] and by M. Eissa and M. Sayed in [14]. The vibration control induced by people walking on  
94 large span composite decks has analysed by Wendell.D Varela and Ronaldo C.Battista [15]. The  
95 efficiency of active vibration control of smart plates using directional actuation and sensing capability  
96 of piezoelectric composite is derived by S.Kapuria, M.Yaqoob Yasin in 2013 [16]. He was applied the  
97 linear quadratic Gaussian control strategy for active vibration control. Recently in 2013, Hesam  
98 Hajheidari, Hamid Reza Mirdamadi, derived the spectral finite element formulation for vibration  
99 analysis of rectangular symmetric cross -ply of laminated composite plates [17]. Khan and Kim [18]  
100 investigate the active vibration control of a piezo-bonded laminated composite in the presence of  
101 sensor partial debonding and structural delamination. They develop an electromechanically coupled  
102 finite-element model and analyze how these damage mechanisms influence the performance of a  
103 constant gain velocity feedback controller. Their results show that sensor debonding degrades  
104 vibration suppression, whereas structural delamination can enhance control authority due to reduced  
105 structural stiffness. Sharma et al. [19] investigated the static and free vibration behavior of smart  
106 curvilinear fiber laminated composite plates with delamination using a first-order shear deformation  
107 theory-based finite element model. Their study demonstrated that delamination significantly reduces  
108 structural stiffness and natural frequencies, while curvilinear fiber paths can mitigate this reduction by  
109 tailoring stiffness distribution. Additionally, the integration of piezoelectric actuators and sensors with  
110 active feedback control was shown to effectively suppress vibration in delaminated smart composite  
111 plates. Liu et al. [20] developed a theoretical and experimental framework for adaptive active vibration  
112 control of composite laminated plates using macro fiber composite (MFC) piezoelectric patches. By

113 incorporating electromechanical coupling effects and implementing a filtered-x least mean square  
114 (FxLMS) algorithm, they demonstrated significant suppression of vibrations near natural frequencies  
115 as well as under multi-frequency and random excitations. Experimental and FEM validations  
116 confirmed the accuracy and effectiveness of the proposed adaptive closed-loop control system.

### 117 **Material uncertainty of the composite structure:**

118 The meaning of uncertainty is the incompleteness in knowledge and the inherent variability of the  
119 structures and its environment. In early 1955, Uncertainty-based design and optimization technique is  
120 derived [21, 22]. Uncertainty in the composite structures under load can be broadly addressed through  
121 material, geometric and structural considerations [23], based on probabilistic design methodology in  
122 1999. In aerospace engineering the meaning of uncertainty is best defined by DeLaurentis & Mavris  
123 (2000) [24]. Probabilistic strength analysis of uncertain rectangular FRP plates using Monte Carlo  
124 simulation is briefly described by Jeong & Shenoi[25]. A non-deterministic approach is applied to  
125 improve robustness of aerospace vehicle and decrease its sensitivity to maintain the stability [26, 27].  
126 The uncertainty based design of aerospace structures is describe in 2004[28, 29]. The non-linear free  
127 vibration analysis of laminates composite with random material properties is also analyzed by Onkar  
128 and Yadav(2004) [30]. He applied the classical laminate theory in the Von Karman views. The effect  
129 of uncertainties on the prediction of fatigue failure of aerospace and mechanical components is  
130 presented by Koutsourelakis et al in 2006 [31]. In 2007 Onkar et al have given an idea on the  
131 probabilistic failure of uncertain laminated composite plates [32]. The effect of uncertainty in  
132 composite material properties on non linear aero-elastic response was studied by Murugan et al (2008)  
133 [33]. The uncertainty in mechanical properties in FRP laminates and its effect in failure prediction is  
134 studied by Lekou & Philippidis in 2008 [34]. A modal for free vibration analysis of laminated  
135 composite which are kept on elastic foundation with random system properties by Lal et al(2008) [35],  
136 they have taken Green Lagrange strain vector for derivation of the nonlinear strain-displacement  
137 relation [36], and the governing equation of motion is based on Hamilton principle.

138 In the year 2009, Sriramula & Chryssanthopoulos have taken an attempt to quantify the  
139 uncertainty in FRP composites and summarize the different stochastic modeling [37], his approach is  
140 based on stochastic computational mechanics approach. Material uncertainty of composite plates and  
141 matrix cracking effect is derived by Gayathri et al in 2010 [38]. Morales et al has derived the finite  
142 element method for active vibration control of uncertain structures they also introduce the fuzzy

143 design method [39]. A stochastic dynamics application system for monitoring the real time material  
144 damage or uncertainty in aerospace structures system is derived by Prudencio et al recently in 2013  
145 [40]. He has given an overview of the experimental data that he was collected, for the damage models.  
146 The problem of uncertainty propagation in composite laminate structures is studied by Conceição et al  
147 (2013). His approach is based on the optimal design of composite structures by using the Uniform  
148 Design Method to achieve a reliability level [41]

149

### 150 **Conclusion and future scope:**

151 The literature reviews of variety of analytical and numerical model for composite laminate plates has  
152 been developed to predict the damage (matrix crack and delamination). Analytical models mostly  
153 considered classical beam, plate and shell theories, extending them to include induced strain actuation.  
154 There are many authors also worked on vibration control with uncertain material properties. Extensive  
155 amount of research works have been carried out on the numerical methods to develop smart finite  
156 element models with extension-bending of piezoelectric coupling using both classical and shear  
157 deformation theories. The second author also had done a great job on vibration control of composite  
158 structure and aircraft structure [42-44]. But there are still needed extensive works on Vibration control  
159 of composite structure when there is some damage or the material properties are uncertain.

160 In this regard the authors are planning to work on the efficient reduced order model of  
161 composite structure and smart structure. It will be helpful to do component wise modeling of real  
162 structure with minimum number of degrees of freedom. The authors are looking for the analysis of  
163 damage structure or structure with uncertain material properties. This will helpful to prevent  
164 catastrophic failure of structure and avoid accident.

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